PAGE: 1 PRINT DATE: 11/29/01

FAILURE MODES EFFECTS ANALYSIS (FMEA) -- CIL HARDWARE

NUMBER: 03-1-0425 -X

MC271-0075-0025

SUBSYSTEM NAME: MAIN PROPULSION

	R	EVISION: 1	11/08/00
PART DATA			
	PART NAME	PART NUMBER	
	VENDOR NAME	VENDOR	NUMBER
LDU	LINE LUO DEGIDO DETUDN	140074 0	075 0040
LRU	: LINE LH2 RECIRC RETURN SENIOR FLEXONICS (KETEMA DIVISION)	8-031168	075-0016 3
LRU	: LINE LH2 RECIRC RETURN SENIOR FLEXONICS (KETEMA DIVISION)	MC271-0 8-031166	075-0024 i-5

EXTENDED DESCRIPTION OF PART UNDER ANALYSIS:

: LINE LH2 RECIRC RETURN

LINE, LH2 RECIRCULATION RETURN, 2 INCH DIAMETER VACUUM JACKETED. (FH12, FH14, FH16).

SENIOR FLEXONICS (KETEMA DIVISION) 8-031167-5

REFERENCE DESIGNATORS: FH12

FH14 FH16

QUANTITY OF LIKE ITEMS: 3

ONE EACH PART NUMBER PER VEHICLE

FUNCTION:

LRU

EACH LINE EXTENDS FROM THE INDIVIDUAL SSME INTERFACE TO THE FLANGES OF THE 4 INCH RECIRCULATION RETURN MANIFOLD. PROVIDES A PATH FOR RETURNING LH2 TO THE ET DURING ENGINE CONDITIONING (LOADING) AND A MEANS TO OFFLOAD RESIDUAL LH2 DURING DUMP. THE LINES HAVE A VACUUM JACKET THAT INCORPORATES A RUPTURE DISK, EVACUATION VALVE, INTEGRAL SUPPORT BRACKET, THERMOCOUPLE GAGE, AND GETTER ASSEMBLY.

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FAILURE MODES EFFECTS ANALYSIS FMEA -- CIL FAILURE MODE

NUMBER: 03-1-0425-02

REVISION#: 1 11/08/00

SUBSYSTEM NAME: MAIN PROPULSION

LRU: LINE LH2 RECIRC RETURN

ITEM NAME: LINE LH2 RECIRC RETURN

CRITICALITY OF THIS
FAILURE MODE: 1/1

FAILURE MODE:

RUPTURE/LEAKAGE DURING LOADING, ASCENT, AND DUMP.

MISSION PHASE: PL PRE-LAUNCH

LO LIFT-OFF

VEHICLE/PAYLOAD/KIT EFFECTIVITY: 102 COLUMBIA

103 DISCOVERY104 ATLANTIS105 ENDEAVOUR

CAUSE:

MATERIAL DEFECT, FATIGUE FAILURE

CRITICALITY 1/1 DURING INTACT ABORT ONLY? NO

REDUNDANCY SCREEN A) N/A

B) N/A

C) N/A

PASS/FAIL RATIONALE:

A)

B)

C)

- FAILURE EFFECTS -

(A) SUBSYSTEM:

HAZARDS ASSOCIATED WITH LEAKAGE OF LH2 IN AFT COMPARTMENT. POSSIBLE LOSS OF CRITICAL ADJACENT COMPONENTS DUE TO CRYOGENIC EXPOSURE. POSSIBLE AFT COMPARTMENT OVERPRESSURIZATION AND FIRE/EXPLOSION HAZARD. LEAKAGE DURING LOADING DETECTABLE USING HAZARDOUS GAS DETECTION SYSTEM (HGDS). DURING ASCENT, DEPLETION OF FUEL RESULTING IN POSSIBLE PREMATURE SSME SHUTDOWN.

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(B) INTERFACING SUBSYSTEM(S):

SAME AS A.

(C) MISSION:

POSSIBLE LOSS OF CREW/VEHICLE.

(D) CREW, VEHICLE, AND ELEMENT(S):

SAME AS C.

(E) FUNCTIONAL CRITICALITY EFFECTS:

NONE.

-DISPOSITION RATIONALE-

(A) DESIGN:

THE RETURN LINE PRESSURE CARRIER, INCLUDING THE GIMBALS, IS CONSTRUCTED OF INCONEL 718. EACH LINE INCORPORATES THREE FLEXIBLE JOINTS (GIMBAL ASSEMBLIES) TO PROVIDE FOR DIFFERENTIAL MOVEMENT BETWEEN THE SSME AND THE RECIRCULATION MANIFOLD. THE GIMBAL ASSEMBLY CONSISTS OF TWO OPPOSITE FORMED FORKS LOCATED 90-DEGREES TO EACH OTHER AND LINKED TOGETHER WITH ENTRAPPED PINS THROUGH A GIMBAL RING. THE GIMBAL JOINTS INCORPORATE MULTI-PLY BELLOWS TO MINIMIZE STRESS LEVELS. THE FLANGE AT THE SSME INTERFACE END INCORPORATES A LEAK DETECTION PORT FOR MEASURING FLANGE JOINT LEAKAGE.

THE OPERATING LIFE FOR THE LINE ASSEMBLIES IS 225 HOURS OF FLOW WHICH IS EQUIVALENT TO THE TOTAL FLOW PERIOD FOR 100 ORBITAL MISSIONS. THEY ARE DESIGNED FOR A MAXIMUM OPERATING PRESSURE OF 55 PSIG AT -423 DEG F AND A FLOW RATE OF 1.5 POUNDS PER SECOND. MAXIMUM STATIC PRESSURE IS 105 PSIG.

THE PROOF PRESSURE FACTOR IS 1.5 AND THE BURST PRESSURE FACTOR IS 2.0. THE PRESSURE CARRIER MEETS THE FRACTURE ANALYSIS REQUIREMENT FOR 400 MISSIONS. STRUCTURAL ANALYSIS INDICATES POSITIVE (GREATER THAN 1.4) MARGINS OF SAFETY FOR ALL CONDITIONS OF LINE OPERATION.

THE PRESSURE CARRIER WILL WITHSTAND AN IMPLOSION PRESSURE OF 40 PSID. THE VACUUM JACKET WILL WITHSTAND AN IMPLOSION PRESSURE OF 22 PSID. THE LINE ASSEMBLY CAN WITHSTAND A PRESSURE SURGE OF 40 TO 50 PSIG IN 200 MILLISECONDS AND A THERMAL CHANGE 70 DEG F TO 200 DEG F AND 70 DEG F TO -423 DEG F.

(B) TEST:

ATP

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EXAMINATION OF PRODUCT

VACUUM JACKET PRESSURE LEAKAGE - 3 MICRONS/DAY; 60 MICRONS MAXIMUM.

PROOF PRESSURE - 158 PSIG.

OPERATIONAL TEST

LINE ASSEMBLIES ARE SUBJECTED TO A MINIMUM OF ONE MOTION ENVELOPE CYCLE WHILE FILLED WITH LN2 AND PRESSURIZED TO 55 PSIG.

TEMPERATURE TEST - PRESSURIZE TO 55 PSIG; EXTERNAL TEMPERATURE STABILIZED AT 200 DEG F FOR 30 MINUTES, MEASURE VACUUM JACKET RISE RATE (3 MICRONS/DAY; 60 MICRONS MAXIMUM).

PRESSURE CARRIER LEAKAGE - AMBIENT: 15 PSID.

CERTIFICATION

EACH OF THE LINE ASSEMBLIES WERE SUBJECTED TO THE FOLLOWING QUALIFICATION TESTS.

VIBRATION - IN ALL THREE AXES, FILLED WITH LH2, AND PRESSURIZED TO 55 PSIG.

SINUSOIDAL SWEEP OVER THE FREQUENCY RANGE OF 5 TO 35 HZ.

RANDOM VIBRATION WAS MAINTAINED AT THE INLET AND OUTLET ENDS FOR 13.3 HRS.

- FLOW TEST TEST FLUID WAS LH2. INLET PRESSURE WAS 55 PSIG, WITH A FLOW RATE OF 1.5 LBS/SEC AND PRESSURE DROP OF LESS THAN 0.75 PSID OVER THE SYSTEM OF LINES.
- ENDURANCE TEST 2000 CYCLES WERE AT 80% ANGULATION; 200 CYCLES WERE AT EXTREME MOTION WHILE FILLED WITH LN2 AND PRESSURIZED TO 55 PSIG.
- PRESSURE CYCLING (ENGINE 1 LINE ONLY) 100 CYCLES; 10 TO 105 PSIG; FILLED WITH LN2; 50 CYCLES WITH LINE 80% EXTENDED AND 50 CYCLES WITH LINE 80% COMPRESSED.
- TEMPERATURE CYCLING TEST (AMBIENT TO -150 DEG F FOR 4 HOURS; TO 275 DEG F FOR 30 MIN; TO AMBIENT).
- 3 CYCLES, LINE FILLED WITH LN2: PRESSURIZED TO 55 PSIG.
- 5 OPERATIONAL ANGULATION CYCLES DURING EACH TEMPERATURE EXTREME.
- HEAT TRANSFER TEST (ENGINE 1 AND 2 ONLY) FILLED WITH LN2; CHAMBER TEMPERATURE 80 DEG F OR GREATER; HEAT TRANSFER 30 BTUS PER HOUR PER SQUARE FOOT OF EXTERNAL SURFACE.

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IMPLOSION TEST - 22 PSID ACROSS VACUUM JACKET FOR 3 MINUTES; VACUUM ANNULUS PRESSURIZED TO 50 PSIG AND HELD FOR 3 MINUTES.

PRESSURE CARRIER LEAKAGE - 14.5 PSI.

VACUUM JACKET LEAKAGE - 500 MICRONS MAXIMUM INCREASE DURING QUALIFICATION TESTS.

BURST TEST - NO LEAKAGE OR DAMAGE AFTER 5 MINUTES AT 210 PSIG.

OMRSD

ANY TURNAROUND CHECKOUT IS ACCOMPLISHED IN ACCORDANCE WITH OMRSD.

(C) INSPECTION:

RECEIVING INSPECTION

RAW MATERIALS ARE VERIFIED BY INSPECTION FOR MATERIALS AND PROCESSES CERTIFICATION.

CONTAMINATION CONTROL

CLEANLINESS TO LEVEL 400 IS VERIFIED BY INSPECTION.

ASSEMBLY/INSTALLATION

COMPONENTS ARE INSPECTED VISUALLY, DIMENSIONALLY, AND INCREMENTALLY DURING FABRICATION. MACHINING OPERATION OF FLANGE DETAIL PARTS IS VERIFIED PER DRAWING AND APPLICABLE SPECIFICATION. DRAWING TORQUE REQUIREMENTS, TOLERANCES, AND SURFACE FINISHES ARE VERIFIED BY INSPECTION. INSPECTION FOR ALIGNMENT AND VACUUM JACKET PRESSURE IS MONITORED AND VERIFIED. ELECTROETCH MARKING IDENTIFICATION OF LINES IS VERIFIED BY INSPECTION. MANDATORY INSPECTION POINTS ARE INCLUDED IN THE ASSEMBLY PROCEDURE.

CRITICAL PROCESSES

WELDING, PARTS PASSIVATION, HEAT TREATMENT, AND ELECTROPOLISH OF TUBING ARE ALL VERIFIED BY INSPECTION. LUBRICATION OF GIMBAL PINS IS VERIFIED.

NONDESTRUCTIVE EVALUATION

ETCHING AND DYE PENETRANT INSPECTION VERIFIED ON ALL MACHINED PARTS. X-RAY AND DYE PENETRANT INSPECTION OF WELDS ARE VERIFIED BY INSPECTION.

TESTING

ATP IS OBSERVED AND VERIFIED BY INSPECTION.

HANDLING/PACKAGING

PACKAGING FOR SHIPMENT IS VERIFIED BY INSPECTION.

(D) FAILURE HISTORY:

CURRENT DATA ON TEST FAILURE, FLIGHT FAILURE, UNEXPLAINED ANOMALIES, AND OTHER FAILURES EXPERIENCED DURING GROUND PROCESSING ACTIVITY CAN BE FOUND IN THE PRACA DATABASE.

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(E) OPERATIONAL USE:

FLIGHT: NO CREW ACTION CAN BE TAKEN.

GROUND: GROUND OPERATIONS SAFING PROCEDURES CONTAIN SAFING SEQUENCE

OF EVENTS FOR MAJOR LEAKS IN THE HYDROGEN SYSTEM.

- APPROVALS -

: /S/ W. P. MUSTY : W.P. MUSTY S&R ENGINEERING

: P. A. STENGER-NGUYEN : /S/ P. A. STENGER-NGUYEN

S&R ENGINEERING
S&R ENGINEERING ITM
DESIGN ENGINEERING
MPS SUBSYSTEM MGR.
MOD
USA SAM
USA ORBITER ELEMENT
NASA SR&QA

: W.F. MIGG.
: W.F. MIGG.
: P. A. STENGER-NGUYEN
: P. A. STENGER-NG
: P. A. STENGER-NG
: /S/ P. A. STENGER-NG
: /S/ EARL HIRAKAWA
: /S/ EARL HIRAKAWA
: /S/ TIM REITH
: /S/ BILL LANE
: /S/ BILL LANE
: /S/ MIKE SNYDER
: /S/ SUZANNE LITTLE
: /S/ SUZANNE LITTLE
: /S/ SUZANNE LITTLE
: /S/ ERICH BASS